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COMPLETE SPECIFICATION

Process for the Production of Alpha-Epichlorhydrin

We, SOLVAY & CIE., a Body Corporate organised under the Laws of Belgium, of 33, rue Prince Albert, Brussels, Belgium, do hereby declare the invention, for which we pray that a patent may be granted to us, and the method by which it is to be performed, to be particularly described in and by the following statement:

The present invention relates to a process for the production of alpha-epichlorhydrin by treating glycerol-dichlorhydrins with basic substances, particularly hydroxides or carbonates of alkali metals or alkaline earth metals.

It is known that the dehydrochlorination of glycerol-dichlorhydrins is accompanied by the saponification of a portion of the epichlorhydrin formed, leading to the formation of glycerol and thus substantially reducing the yield in epichlorhydrin.

In order to obviate this disadvantage, it has been proposed to remove the epichlorhydrin as and when it is formed by distilling the reaction mixture at such a rate that the vapours carried over contain not only epichlorhydrin, but also water and dichlorhydrins. From the condensed vapours the insoluble epichlorhydrin is isolated whilst the aqueous phase containing the unreacted dichlorhydrin is recycled to the dehydrochlorination apparatus.

The dehydrochlorination and the distillation are preferably effected in columns divided into compartments, or in tubular apparatus so as to obviate a continuous mixing of the reaction mass. On the other hand, high yields in epichlorhydrin are only obtained when effecting the distillation under reduced pressure.

It has now been found that epichlorhydrin may be produced in a continuous process by reacting a basic substance with an aqueous mixture of glycerol dichlor-

hydrins in the presence of a water-immiscible solvent of epichlorhydrin which circulates in counter-current to the aqueous phase whereby the epichlorhydrin is separated from the solvent outside the dehydrochlorination apparatus and the solvent is continuously recycled to the dehydrochlorination apparatus for a fresh extraction of epichlorhydrin.

All organic compounds which dissolve epichlorhydrin and are water-insoluble may be used as solvents according to the process of the invention. Solvents of this kind are for example hydrocarbons such as benzene, toluene, xylenes; halogenated hydrocarbons such as carbon tetrachloride, trichlorethylene, perchlorethylene, chloropropenes, chloropropanes, and more particularly 1,2,3-trichloropropane, chlorobutanes, chlorobenzenes; ether-oxides such as butyric or amylic ether; ketones such as methylpropylketone, ethylpropylketone, amylmethylketone, 5-methylhexanone, amylethylketone, or esters such as alpha-methyl-propyl acetate, butyl or amyl propionate.

The dehydrochlorination and the continuous extraction of epichlorhydrin thus formed are preferably carried out in an extraction column having compartments for example a Scheibel column containing consecutive compartments for decantation and agitation.

The introduction of the basic agent may be effected after mixing the requisite quantity with the dichlorhydrins in an aqueous medium, by simultaneous introduction with the latter, or also by introduction at several points of the height of the dehydrochlorination apparatus so as to obviate too strong local concentrations of the basic agent which assist the hydrolysis of epichlorhydrin to form glycerol monochlorhydrin, glycidol, or glycerol.

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The attached drawing shows diagrammatically the production cycle of epichlorhydrin according to the process of the invention applied to the special case of a solvent which is heavier than water and whose boiling point is between that of epichlorhydrin and glycerol dichlorhydrins. Such a solvent is for example 1,2,3-trichloropropane, a by-product of the production of dichlorhydrins by hypochlorination of allyl chloride.

Into a column 1, having compartments, used as apparatus for the dehydrochlorination and extraction, there is introduced at the bottom the aqueous solution of glycerol dichlorhydrins from the tank A, and a portion of the basic agent in an aqueous solution from the tank B. The remaining basic agent required for the dehydrochlorination is introduced at an intermediate level of the column 1.

The solvent from the tank C is introduced at the top of the column 1.

The epichlorhydrin is extracted as and 25 when it is formed and is dissolved in the solvent. The unreacted dichlorhydrins are likewise dissolved in the organic solvent so that the aqueous phase leaving at the top of the extraction column at 6 practically 30 contains only chloride and excess basic agent. The organic phase containing the solvent, epichlorhydrin, glycerol-dichlorhydrins and a little water is introduced through the pipe 7 into the distillation column 2 where it is subjected to drying 35 by azeotropic distillation.

The epichlorhydrin and water leaving at the head of the column are condensed in the condensers 8 and 9. One portion 40 flows back to the column, whilst the other is separated into two layers in the Florentine flask 3. The bottom layer formed by epichlorhydrin is returned to the column 2 through the pipe 10, whilst 45 the top layer formed by water and some dissolved epichlorhydrin is returned through the pipe 11 to the dehydrochlorination and extraction column 1.

Since the aqueous solutions of dichlorhydrins obtained by hypochlorination of allyl chloride still contain a small amount of the latter compound, it is conducted to the head of the column 2 and may itself be used for the azeotropic removal of 55 water. If desired, it is possible to add further quantities of allyl chloride or another azeotropic agent for removal.

The solution of epichlorhydrin and dichlorhydrins in the organic solvent is 60 discharged through the pipe 12 into the distillation column 4 at the head of which epichlorhydrin is separated and removed from the cycle through the pipe 13.

The solvent collected at the bottom of 65 the column 4 is freed from dissolved

dichlorhydrins by treating with water in counter-current in the extraction column 5. The practically pure solvent is returned to storage through the pipe 14, whilst the aqueous solution of dichlorhydrins is returned through the pipe 16 into a compartment of the extraction column 1 where the dichlorhydrins concentration is approximately the same as that of the re-cycled solution. 75

The use of a solvent having a high boiling point has the advantage of avoiding the consumption of energy required for the evaporation of the solvent the volume of which is usually large in 80 relation to that of the solute.

However, when the boiling point of the solvent is comprised between that of epichlorhydrin and those of the dichlorhydrins, it may be important to rectify 85 a portion of the solvent which is re-cycled at the top of the extraction column 1, and to re-introduce the remainder containing the dichlorhydrins at a carefully selected height of the extraction and dehydro-90 chlorination column.

When using a solvent whose boiling point is below that of epichlorhydrin, for example carbon tetrachloride, the components of the organic phase may be 95 separated by rectification.

If the solvent forms an azeotrope with epichlorhydrin the organic phase is subjected to rectification and the azeotropic mixture thus obtained at the head of the 100 column is separated by extraction in the presence of a third solvent, for example water. This is particularly the case when the solvent is monochlorobenzene.

Generally speaking, the solution of epichlorhydrin and dichlorhydrins in any solvent may be treated with water to separate the solvent. This process may be of importance when it is desired to separate a portion or the total of the 110 epichlorhydrin in the glycerol-mono-chlorhydrin state.

The following Example is given for the purpose of illustrating the invention.

EXAMPLE

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Into a reactor formed by a seven tier extraction column, each tier comprising a compartment for decantation and a compartment for stirring, there are introduced at the bottom (first tier) 294 litres per 120 hour of an aqueous glycerol-dichlorhydrin containing 0.316 mole per litre, i.e., 93 mole per hour.

This solution also contains sodium chloride at a concentration of 0.392 mole 125 per litre, i.e., an addition of 144 mole per hour.

30 Litres per hour of an aqueous solution of 5N sodium hydroxide solution are introduced into the reactor, the distri- 130

bution being 20 litres per hour at the first tier and 10 litres per hour at the third tier. At the head of the column there are introduced 56.3 litres per hour (78.4 5 kilograms per hour) of 1,2,3-trichloropropane.

The epichlorhydrin formed during the dehydrochlorination as well as a portion of the unreacted dichlorhydrins are 10 absorbed by trichloropropane.

The residual water removed at the top of the column carries away 2.05 mole of glycerol, 3.8 mole of glycerol-dichlorhydrins, 235 mole of sodium chloride and 15 59 mole of excess sodium hydroxide per hour.

The organic phase leaving the column through the pipe 7 contains epichlorhydrin and dichlorhydrins at a concentration of 0.111 and 0.050 mole per 100 grams of solvent respectively.

This solvent is dried in the distillation column 2 by the azeotropic removal of water by epichlorhydrin. The water 25 which has dissolved some epichlorhydrin is re-cycled to the reactor through the pipe 11. The organic phase separated in the Florentine flask 3 is returned to the distillation column 2. At the bottom of 30 this column the dry solvent is withdrawn from which the epichlorhydrin is separated by rectification in the column 4. 87 Mole per hour of epichlorhydrin are continuously discharged at 13.

35 The solvent containing unreacted dichlorhydrins is treated in an extraction column 5 having four tiers and contacted in counter-current with a water supply of 150 litres per hour, the water being introduced at the bottom of the column at 15. The aqueous solution of dichlorhydrins at a concentration of 0.26 mole per litre is re-introduced into the extraction column 1 at the third tier.

45 The yield of epichlorhydrin referred to dichlorhydrins is 93.5 per cent of the

theoretical.

WHAT WE CLAIM IS:—

1. Process for the continuous production of alpha-epichlorhydrin by the 50 reaction of a basic substance with an aqueous mixture of glycerol-dichlorhydrins, characterised by working in the presence of a water-immiscible solvent of epichlorhydrin which circulates in 55 counter-current to the aqueous phase, the epichlorhydrin being separated from the solvent outside the dehydrochlorination apparatus, and the solvent being continuously re-cycled to the dehydrochlorination apparatus for a fresh extraction of epichlorhydrin.

2. Process according to Claim 1 characterised in that the solvent is 1,2,3-trichloropropane. 65

3. Process according to Claim 1 or 2, characterised by introducing the basic agent at several points of the reactor.

4. Process according to any of the preceding claims characterised by separating epichlorhydrin from the solvent by rectification, and by treating the solution of dichlorhydrins in the solvent with water whereby the aqueous phase is re-cycled to the lower part and the organic 75 phase to the upper part of the reactor.

5. Process according to Claim 1 characterised in that the solvent has a lower boiling point than epichlorhydrin.

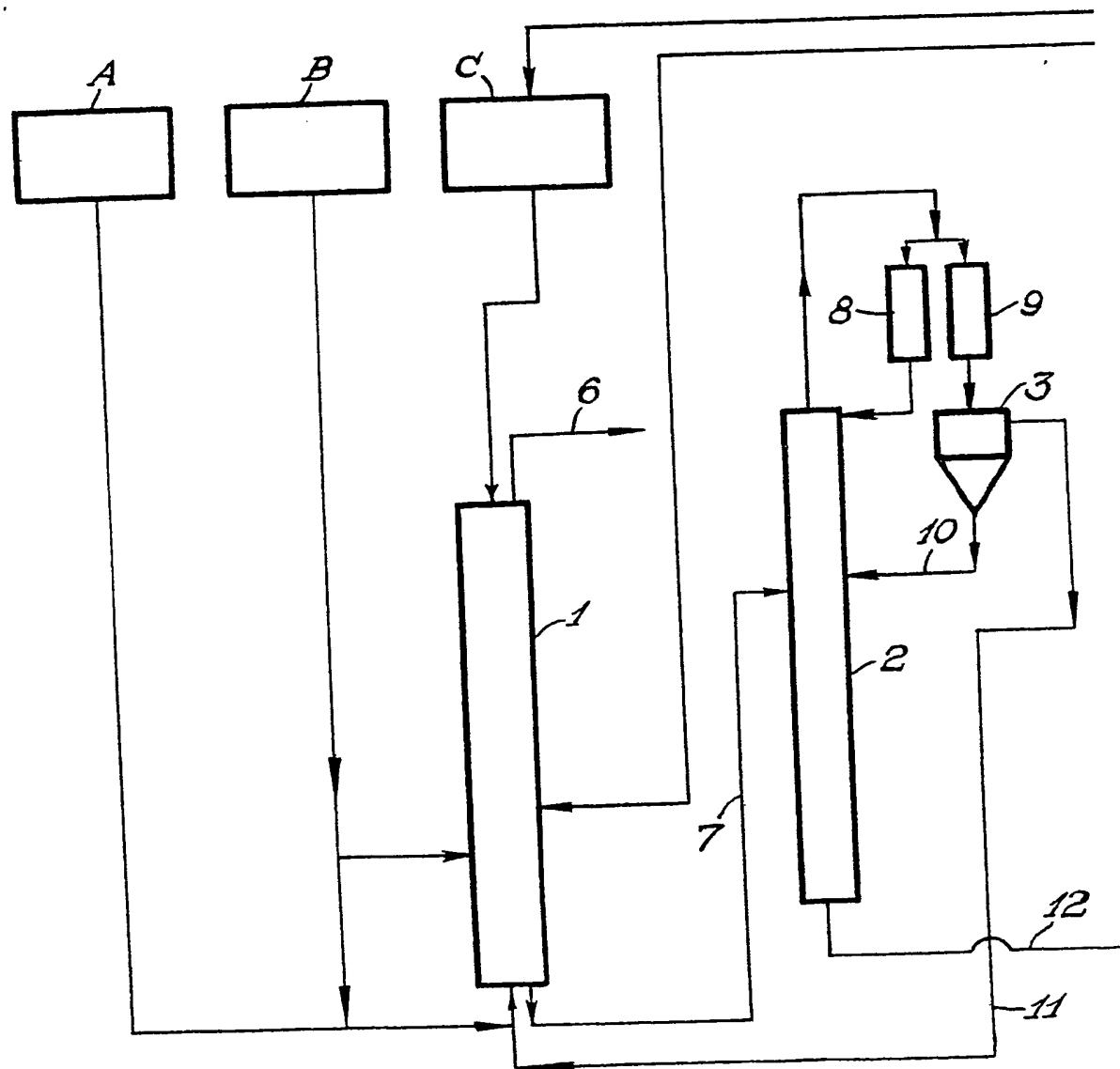
6. Process according to Claim 1 characterised in that the solvent forms an azeotrope with epichlorhydrin.

7. Epichlorhydrin obtained by a process according to any of the preceding claims.

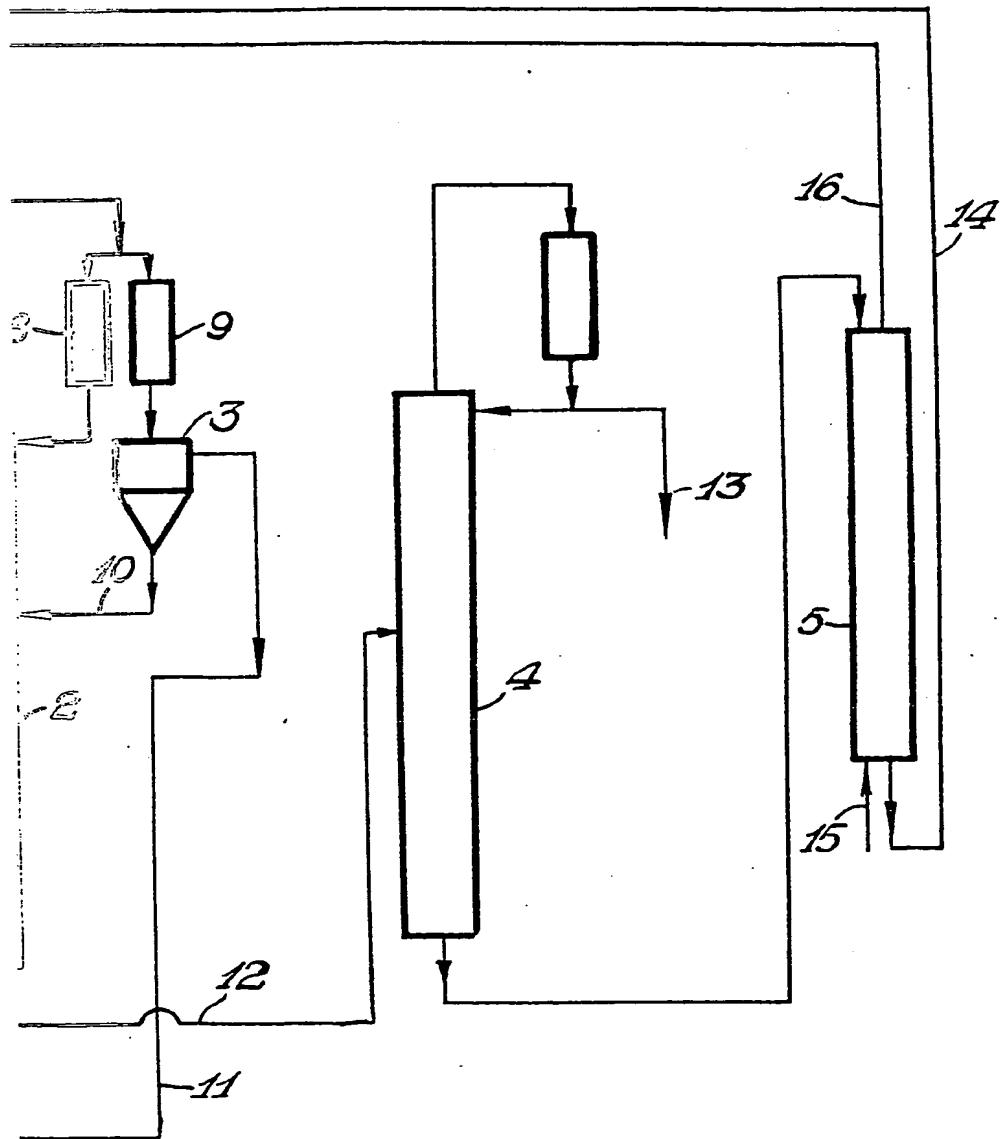
8. Process according to Claim 1 substantially as described in the foregoing Example.

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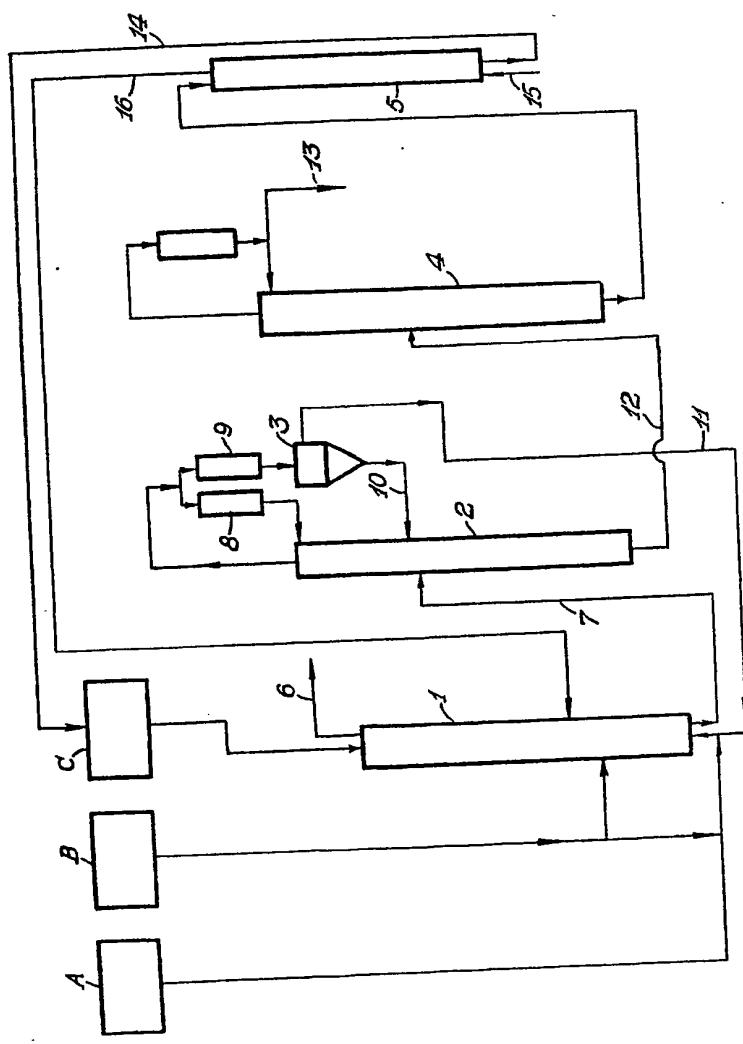
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